2-Phase Stepper Motor Unipolar Driver ICs

■Absolute Maximum Ratings

(Ta=25°C)

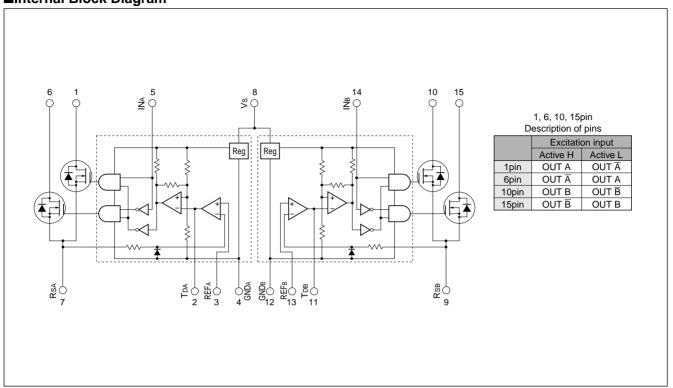
			11. %			
Parameter	Symbol	SLA7022MU	SLA7029M	SMA7022MU	SMA7029M	Units
Motor supply voltage	Vcc		V			
FET Drain-Source voltage	Voss		V			
Control supply voltage	Vs		V			
TTL input voltage	Vin		V			
Reference voltage	V _{REF}		V			
Output current	lo	1 1.5		1	1.5	A
Power dissipation	P _{D1}	4.5 (Withou	ut Heatsink)	4.0 (Withou	W	
	P _{D2}	35 (Tc:	=25°C)	28(Tc=	W	
Channel temperature	T _{ch}		°C			
Storage temperature	T _{stg}		°C			

■Electrical Characteristics

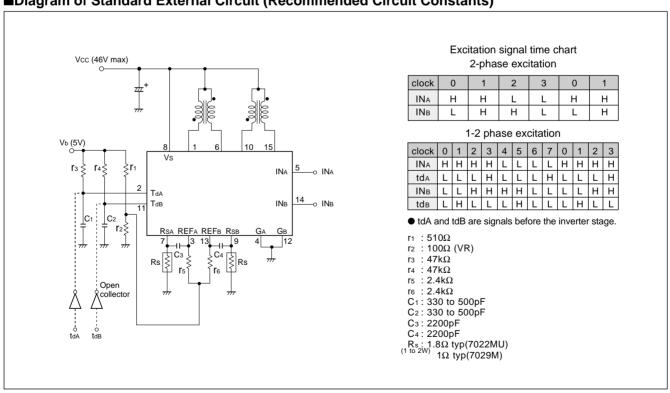
(Ta=25°C)

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							Rati	ings								
Parameter	Symbol	SLA7022MU		SLA7029M		SMA7022MU			SMA7029M			Units				
		min	typ	max	min	typ	max	min	typ	max	min	typ	max			
Control supply current	Is		10	15		10	15		10	15		10	15	mA		
	Condition		Vs=44V			Vs=44V			Vs=44V			Vs=44V				
Control sup	ply voltage	Vs	10	24	44	10	24	44	10	24	44	10	24	44	V	
FET Drain-S	Source	V _{DSS}	100			100			100			100			V	
voltage		Condition	Vs=44V, IDSS=250 μA		Vs=44V, I _{DSS} =250 μA		Vs=44V, IDSS=250 μA		Vs=44V, I _{DSS} =250 μA) v					
FET ON voltage	VDS			0.85			0.6			0.85			0.6	V		
	Condition	l _D =	=1A, Vs=1	I4V	ID=	1A, Vs=1	4V	lo=	=1A, Vs=1	14V	l _D =	=1A, Vs=	14V	v		
FET drain leakage current	IDSS			4			4			4			4	mA		
	Condition	VDSS	=100V, V	's=44V	Voss	=100V, V	s=44V	Voss	=100V, V	/s=44V	VDSS	=100V, V	s=44V	IIIA		
를 FET diode f	FET diode forward	Vsp			1.2			1.1			1.2			1.1	V	
voltage		Condition		ID=1A			ID=1A			l⊳=1A			ID=1A			
Irac	20	Ін			40			40			40			40	μΑ	
FET diode forward voltage TTL input current	Condition	V _{IH} =	=2.4V, Vs=	=44V	V _{IH} =	2.4V, Vs=	=44V	V _{IH} =	2.4V, Vs	=44V	V _{IH} =	2.4V, Vs	=44V	μΑ		
	lıL			-0.8			-0.8			-0.8			-0.8	mA		
		Condition	VIL=	=0.4V, Vs=	=44V	VIL=	0.4V, Vs=	=44V	Vıl=	0.4V, Vs	=44V	VIL=	0.4V, Vs	=44V	IIIA	
	TTL input voltage (Active High)	ViH	2			2			2			2				
TTL input v		Condition		I _D =1A			ID=1A			I⊳=1A			ID=1A		V	
(Active High		VIL			0.8			0.8			0.8			0.8	_	
	Condition	,	VDSS=100	V	\	/DSS=100\	V	,	V _{DSS} =100	V	,	V _{DSS} =100	V			
TTL input voltage	ViH	2			2			2			2			- V		
	Condition	,	VDSS=100	V	١	/DSS=100	V	,	V _{DSS} =100	V	,	V _{DSS} =100	V			
(Active Lov	(Active Low)	VIL			0.8			0.8			0.8			0.8	v	
	Condition		ID=1A			ID=1A			I⊳=1A			ID=1A				
AC characteristics Switching time	Tr		0.5			0.5			0.5			0.5		1		
	Condition	Vs=	Vs=24V, ID=0.8A		Vs=24V, In=1A		Vs=24V, ID=0.8A		Vs=24V, In=1A							
	Tstg		0.7			0.7			0.7			0.7		μs		
	Condition	Vs=	=24V, ID=0).8A	Vs=24V, In=1A		Vs=24V, ID=0.8A		Vs=24V, In=1A			μ δ				
	Tf		0.1			0.1			0.1			0.1				
ĕ	¥	Condition	Vs=	=24V, Id=(D.8A	Vs	=24V, ID=	:1A	Vs=	=24V, ID=	0.8A	Vs	=24V, Id=	=1A		

■Internal Block Diagram

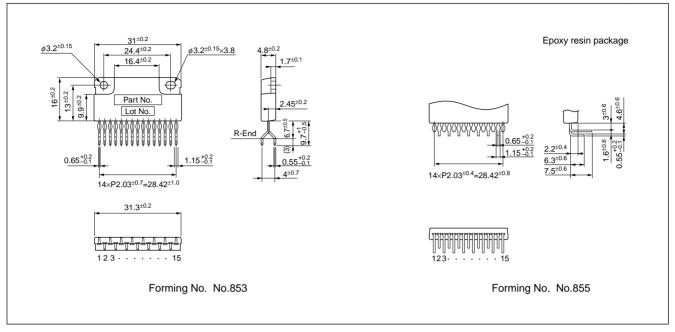


■Diagram of Standard External Circuit (Recommended Circuit Constants)



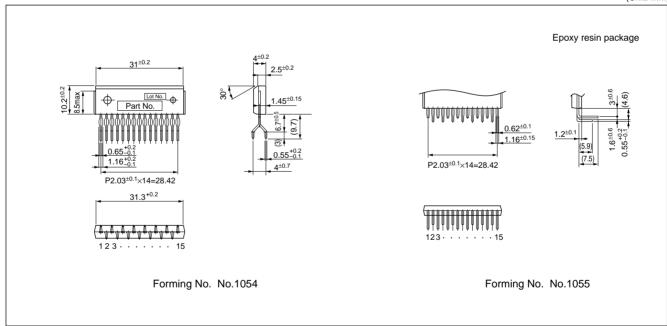
■External Dimensions SLA7022MU/SLA7029M

(Unit: mm)



■External Dimensions SMA7022MU/SMA7029MA

(Unit: mm)



Application Notes

■Determining the Output Current

Fig. 1 shows the waveform of the output current (motor coil current). The method of determining the peak value of the output current (Io) based on this waveform is shown below.

(Parameters for determining the output current lo)

V_b: Reference supply voltage

r₁,r₂: Voltage-divider resistors for the reference supply voltage

Rs: Current sense resistor

(1) Normal rotation mode

lo is determined as follows when current flows at the maximum level during motor rotation. (See Fig.2.)

$$I_0 \cong \frac{r_2}{r_1 + r_2} \bullet \frac{V_b}{R_s} \tag{1}$$

(2) Power down mode

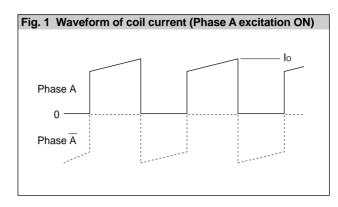
The circuit in Fig.3 (rx and Tr) is added in order to decrease the coil current. lo is then determined as follows.

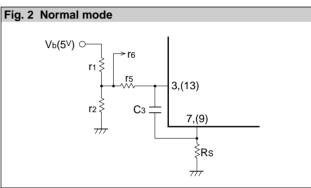
$$I_{\text{OPD}} \cong \frac{1}{1 + \frac{r_1(r_2 + r_X)}{r_2 \bullet r_X}} \bullet \frac{V_b}{R_s} \qquad (2)$$

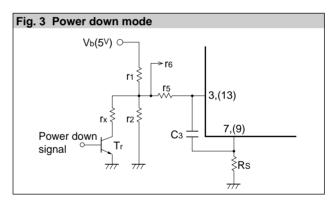
Equation (2) can be modified to obtain equation to determine rx.

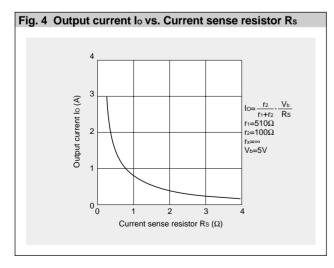
$$rx = \frac{1}{\frac{1}{r_1} \left(\frac{V_b}{R_s \bullet l_{OPD}} - 1 \right) - \frac{1}{r_2}}$$

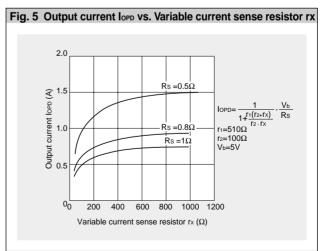
Fig. 4 and 5 show the graphs of equations (1) and (2) respectively.











(NOTE)

Ringing noise is produced in the current sense resistor Rs when the MOSFET is switched ON and OFF by chopping. This noise is also generated in feedback signals from Rs which may therefore cause the comparator to malfunction. To prevent chopping malfunctions, r₅(r₆) and C₃(C₄) are added to act as a noise filter.

However, when the values of these constants are increased. the response from Rs to the comparator becomes slow. Hence the value of the output current lo is somewhat higher than the calculated value.

■Determining the chopper frequency

Determining Toff

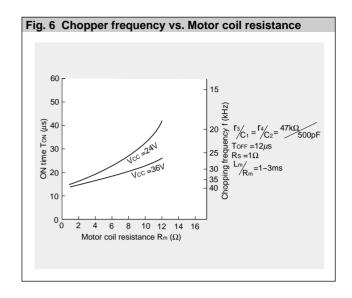
The SLA7000M and SMA7000M series are self-excited choppers. The chopping OFF time T_{OFF} is fixed by r_3/C_1 and r_4/C_2 connected to terminal Td.

Toff can be calculated using the following formula:

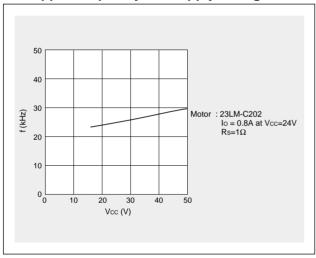
$$\mathsf{Toff} \cong \mathsf{-r}_3 \bullet \mathsf{C}_1 \ell_n \big(1 - \frac{2}{\mathsf{V}_b} \, = \! -\mathsf{r}_4 \bullet \mathsf{C}_2 \, \ell_n \big(1 - \frac{2}{\mathsf{V}_b} \big)$$

The circuit constants and the Toff value shown below are recommended.

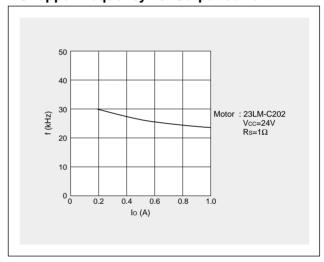
Toff = $12\mu s$ at r_3 = $47k\Omega$, C_1 =500pF, V_b =5V



■Chopper frequency vs. Supply voltage



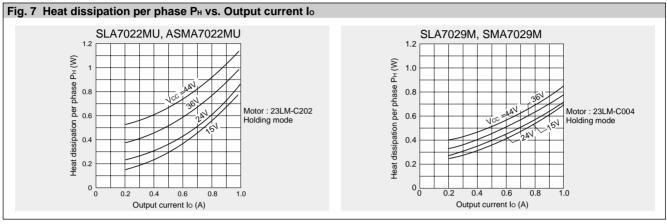
■Chopper frequency vs. Output current

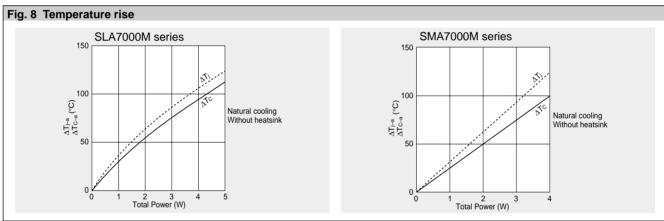


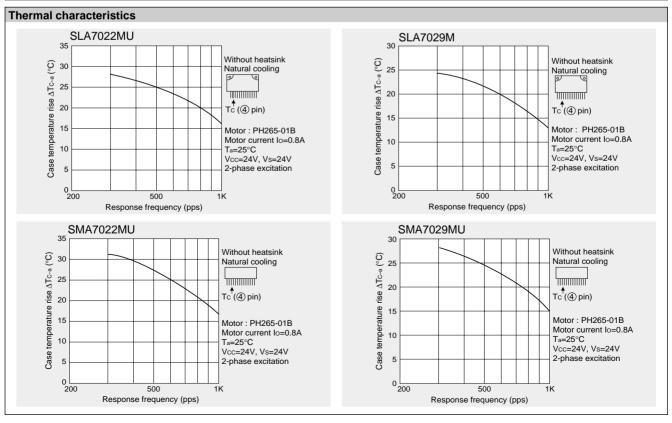
■Thermal Design

An outline of the method for calculating heat dissipation is shown below. (1)Obtain the value of PH that corresponds to the motor coil current lo from Fig. 7 "Heat dissipation per phase PH vs. Output current lo."

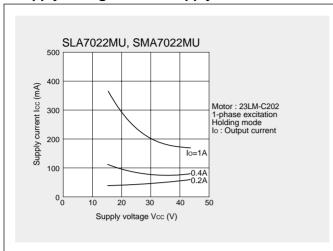
- (2) The power dissipation Pdiss is obtained using the following formula. 2-phase excitation: Pdiss ≅ 2PH+0.015×Vs (W) 1-2 phase excitation: $P_{\text{diss}} \cong \frac{3}{2} P_{\text{H}} + 0.015 \times V_{\text{S}}$ (W)
- (3) Obtain the temperature rise that corresponds to the calculated value of Pdiss from Fig. 8 "Temperature rise."

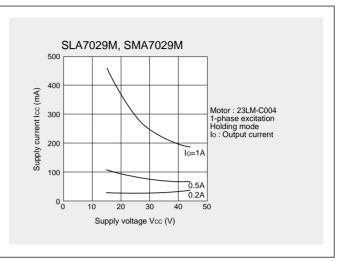




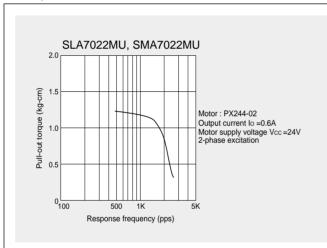


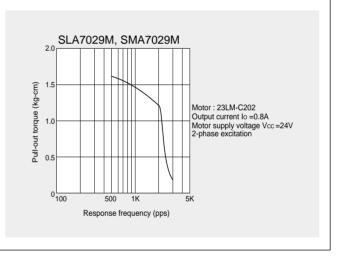
■Supply Voltage Vcc vs. Supply Current Icc





■Torque Characteristics





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